basics, measurement and modelling of BRTF

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Outline

name

- BRTF = bidirectional reflection transmission function
- BSDF = bidirectional scatter distribution function
- Bxxx = .. whatever..

all the same quantity:
scattering of light at a surface

what is this talk about ?

- sequence to simulation results:
  1. measure materials
  2. model material
  3. add geometry, sky, etc
  4. use model in simulation
- why bother measuring at all ?
  1. measured data better then assumptions
  2. no generic BRTF per type of material
     BRTF depends on surface finish
  3. manufacturers specs not always available
  4. recheck manufacturers specs
  5. compare materials by BRTF data

solid angle

- solid angle of an object as seen from point P:
  project object onto sphere with radius r around P
  $\Omega := \frac{A_p}{r^2}$
- unit: *steradian* [sr]
- dimensionless, full sphere: 4π, hemisphere: 2π
- infinitesimal: $d\Omega$, finite: Ω or $\Delta\Omega$
- solid angle of a cone with opening angle α:
  $\Omega_{cone} = 2\pi\left(1 - \cos\frac{\alpha}{2}\right)$

radiant power

basic unit:
power transported by electromagnetic radiation

as described within concept of *photometry*
(sometimes known as *radiance flux*)

three spectral flavours:

- spectrally integrated: *radiometric* [Watt]
- spectrally resolved: power per wavelength interval [Watt/nm]
- weighted by eye response and integrated: *photometric* [Lumen]

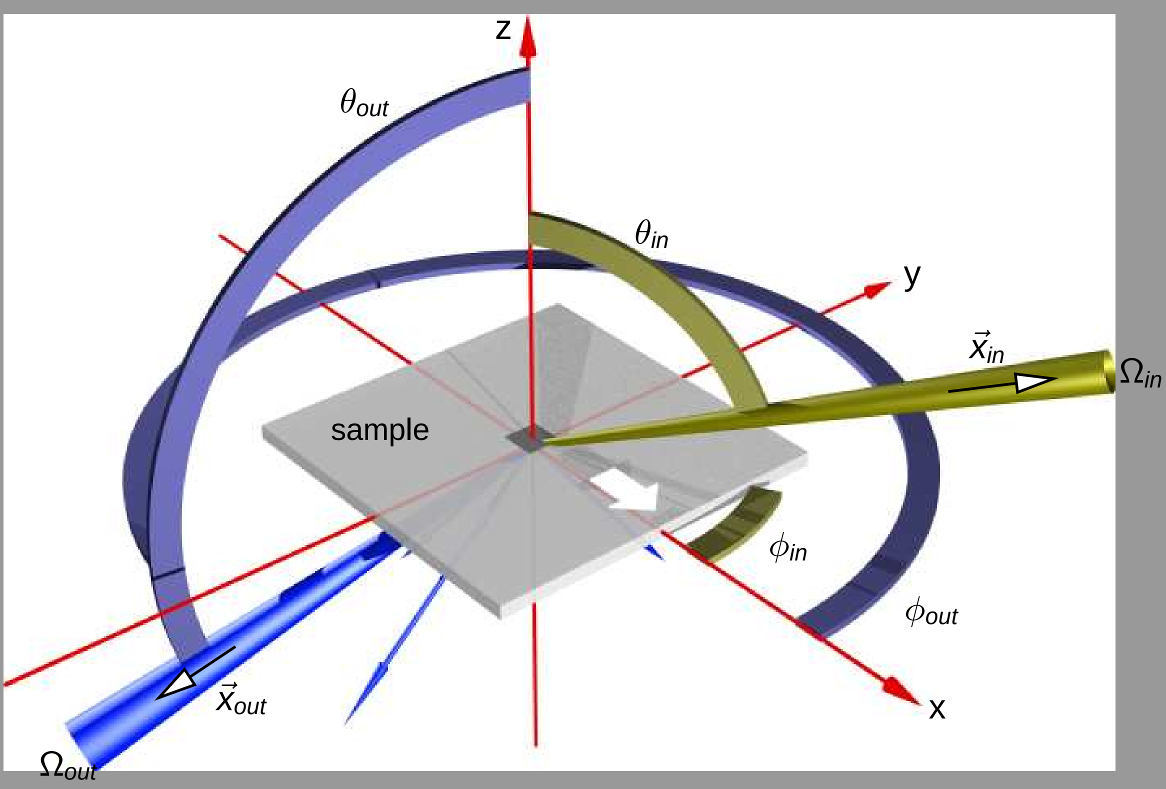
derived quantities

quantities used most often:

- radiant power per area: $\mathcal{E}$ [Watt/m2]
- radiant power per solid angle [Watt/sr] (*Radiant Intensity*)
- radiant power per solid angle and projected area, $\mathcal{L}(\vec{x})$, [Watt/(sr*m^2)] (*Radiance*)

... and equivalent photometric units

coordinate system



coordinate system

advantages of using these sample coordinates:

- standard polar coordinates
- one BRTF for front and back side of sample
- z-axis: surface normal
  x-axis: marked on sample
- direction written as $\vec{x}$ or (θ, ϕ)

With incident light on the *front* surface: $\theta_{in} = (0^o...90^o)$:

- $\theta_{out} = (0^o...90^o)$ reflection,
  $\theta_{out} = (90^o...180^o)$ transmission.

Other coordinates possible, use transformations.

demo

it's all easy ...

defining formula

Definition

$$\mathcal{L}_{out}(\vec{x}_{out}) = \int_{\vec{x}_{in}}^{\Omega_{in}=2\pi} BRTF(\vec{x}_{out}, \vec{x}_{in})\ \mathcal{L}_{in}(\vec{x}_{in})\ \cos(\alpha_{in})\ d\Omega_{in}$$

- $\mathcal{L}_{in}$: incident radiance from $\vec{x}_{in}$
- $d\Omega_{in}$: solid angle of incident light
- $\cos(\alpha_{in})$: historic nuisance (*Lambert* scatterer)
- $\int_{\vec{x}_{in}}^{\Omega_{in}=2\pi}$: integral over hemisphere
- $\mathcal{L}_{out}$: outgoing radiance to $\vec{x}_{out}$
- $BRTF > 0$ and may be > 1
- $BRTF_{void}(\vec{x}_{out}, \vec{x}_{in}) = \delta(\vec{x}_{out} - \vec{x}_{in}) / \cos(\alpha_{in})$, *Dirac Delta function*
- $BRTFc(\vec{x}_{out}, \vec{x}_{in}) := BRTF(\vec{x}_{out}, \vec{x}_{in}) \cos(\alpha_{in})$

approximate formula

$$\mathcal{L}_{out}(\vec{x}_{out}) = \int_{\vec{x}_{in}}^{\Omega_{in}=2\pi} BRTF(\vec{x}_{out}, \vec{x}_{in})\ \mathcal{L}_{in}(\vec{x}_{in})\ \cos(\alpha_{in})\ d\Omega_{in} \qquad (1)$$

- assume $\mathcal{L}_{in} > 0$ for small Ω_{in} around $\vec{x}^*_{in}$ only
- and assume $BRTF = const$ over Ω_{in}
- then, and only then

$$BRTF(\vec{x}_{out}, \vec{x}^*_{in}) \approx \frac{\mathcal{L}_{out}(\vec{x}_{out})}{\mathcal{E}_{in}} \qquad (2)$$

But:
This approximation is misleading and should be used with caution.

averaged BRTF

measured BRTF is always averaged over solid angles of detector $\Delta\Omega_{out}$ and lamp $\Delta\Omega_{in}$:

$$\overline{BRTF}(\Delta\Omega_{in}, \Delta\Omega_{out}) := \frac{1}{\Delta\Omega_{in}\,\Delta\Omega_{out}} \int_{\vec{x}_{out}}^{\Delta\Omega_{out}} \int_{\vec{x}_{in}}^{\Delta\Omega_{in}} BRTF(\vec{x}_{out}, \vec{x}_{in})\; d\Omega_{in}\, d\Omega_{out} \qquad (3)$$

consequences:

this limit measurement of BRTF features.
$\rightsquigarrow$ minimise $\Delta\Omega_{out}$ and $\Delta\Omega_{in}$

transmission values from BRTF

transmission τ from Ω_{in} into Ω_{out} is given by:

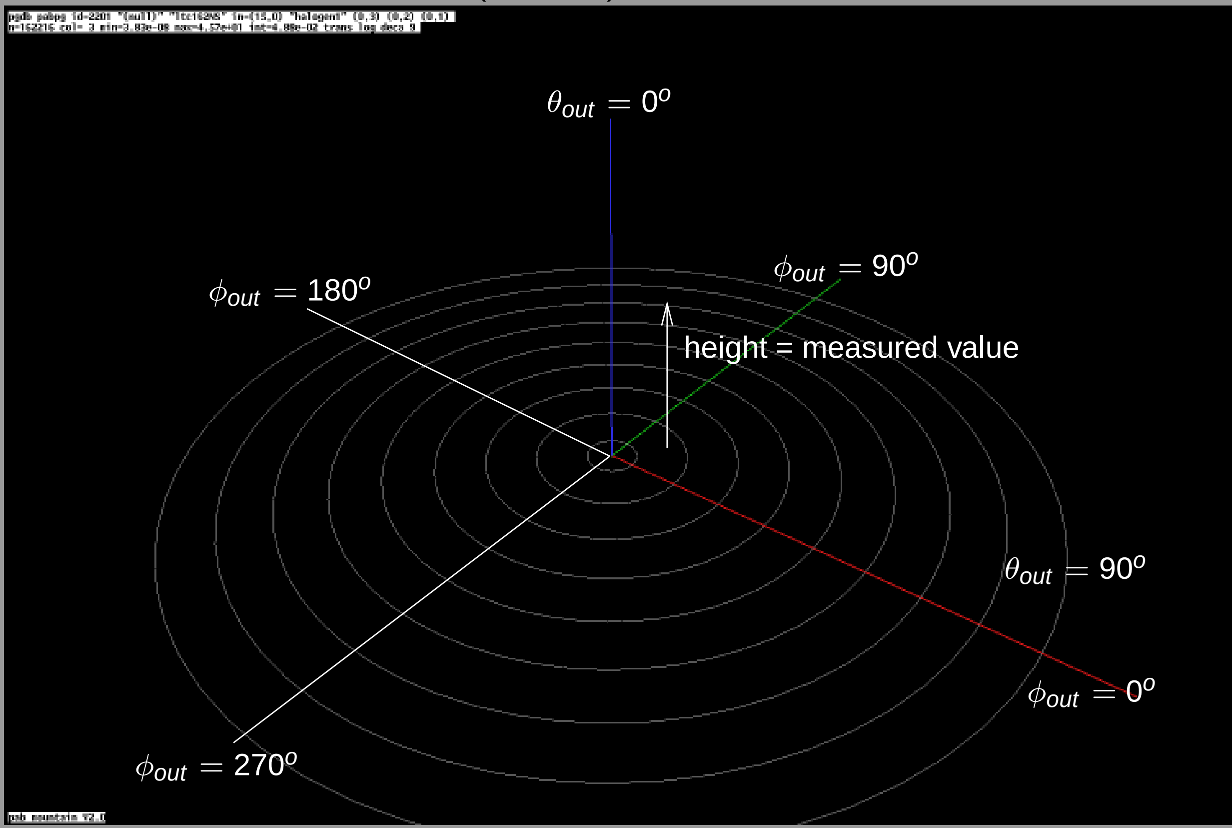
$$\tau(\Omega_{in}, \Omega_{out}) = \frac{\int_{\vec{x}_{out}}^{\Omega_{out}} \left\{ \int_{\vec{x}_{in}}^{\Omega_{in}} BRTF(\vec{x}_{out}, \vec{x}_{in}) \mathcal{L}_{in}(\vec{x}_{in}) \cos(\alpha_{in}) d\Omega_{in} \right\} \cos(\alpha_{out}) d\Omega_{out}}{\int_{\vec{x}_{in}}^{\Omega_{in}} \mathcal{L}_{in}(\vec{x}_{in})\; \cos(\alpha_{in})\; d\Omega_{in}} \qquad (4)$$

Which for the *direct-hemispherical transmission* results in:

$$\tau_{dh}(\vec{x}_{in}) := \tau(d\Omega_{in}, 2\pi) = \int_{\vec{x}_{out}}^{2\pi} BRTF(\vec{x}_{out}, \vec{x}_{in})\; \cos(\alpha_{out}) d\Omega_{out} \qquad (5)$$

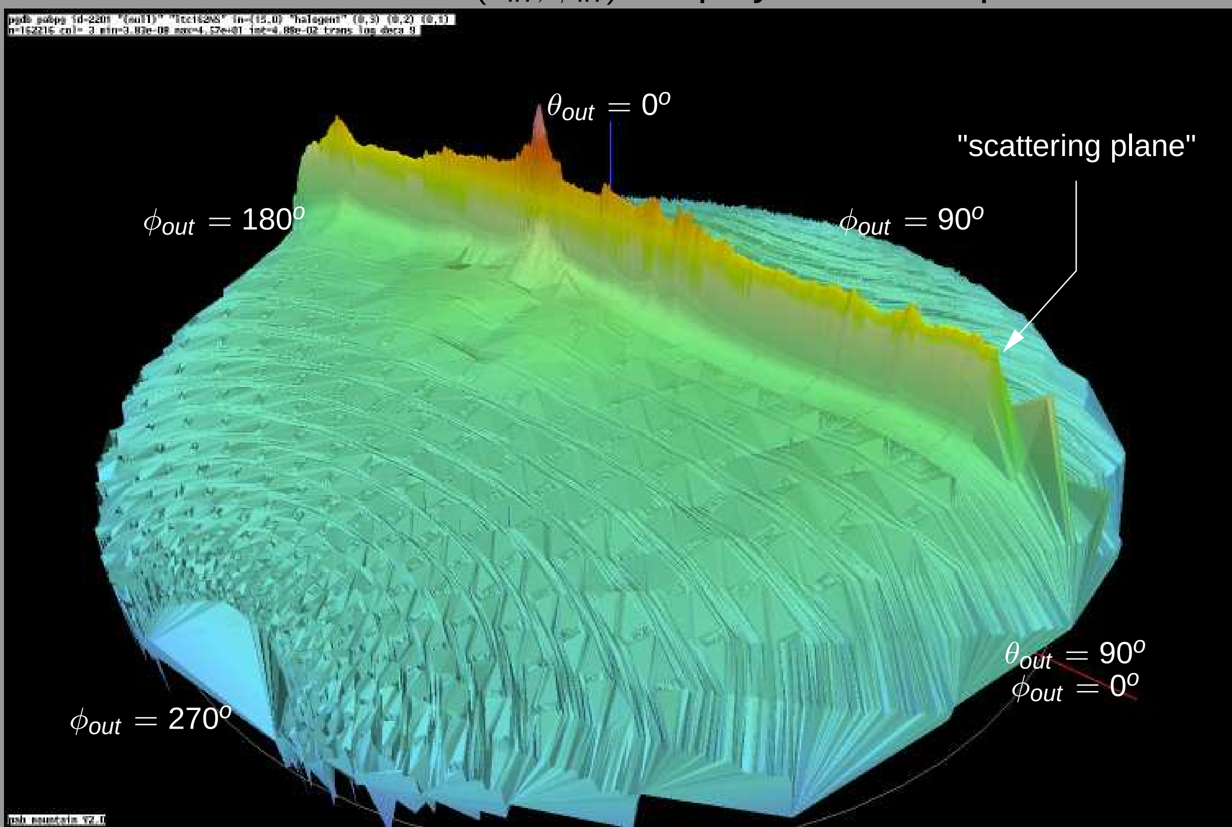
visualising BRTF 3D

for one incident direction (θ_{in}, ϕ_{in}), display one hemisphere:



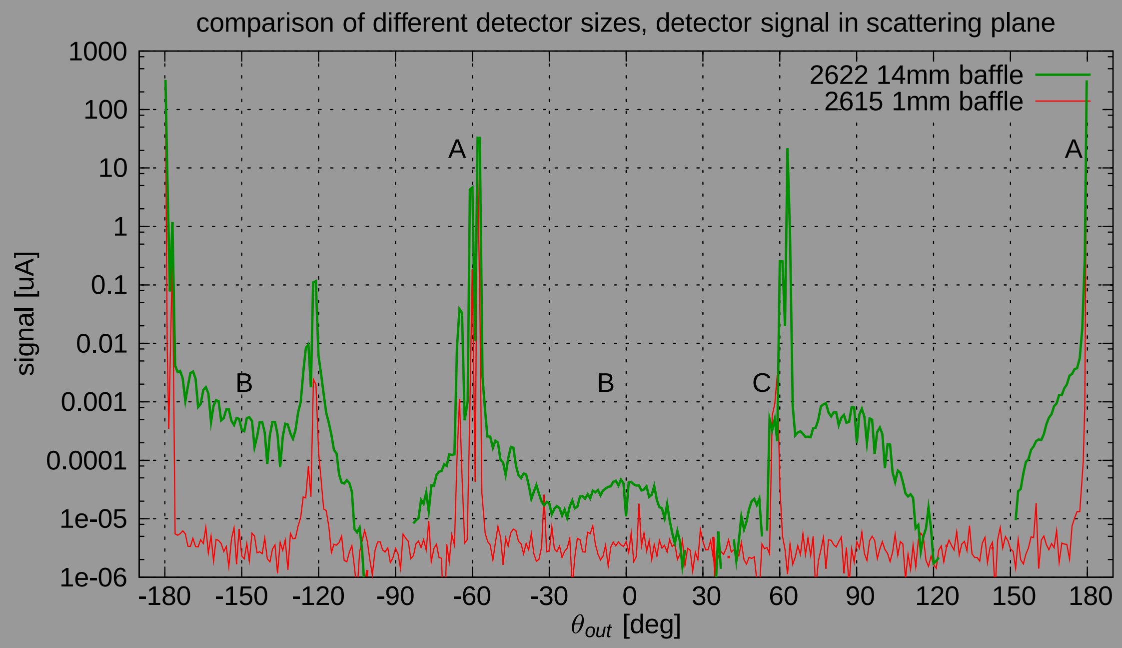
visualising BRTF 3D

for one incident direction (θ_{in}, ϕ_{in}), display one hemisphere:



visualising BRTF 2D

2D cuts along scattering plane through 3D dataset
I prefer Cartesian plots over polar plots. example:



medium sized intermission

... questions to math part ?

next to come: gonio-photometers

light source types & parameters

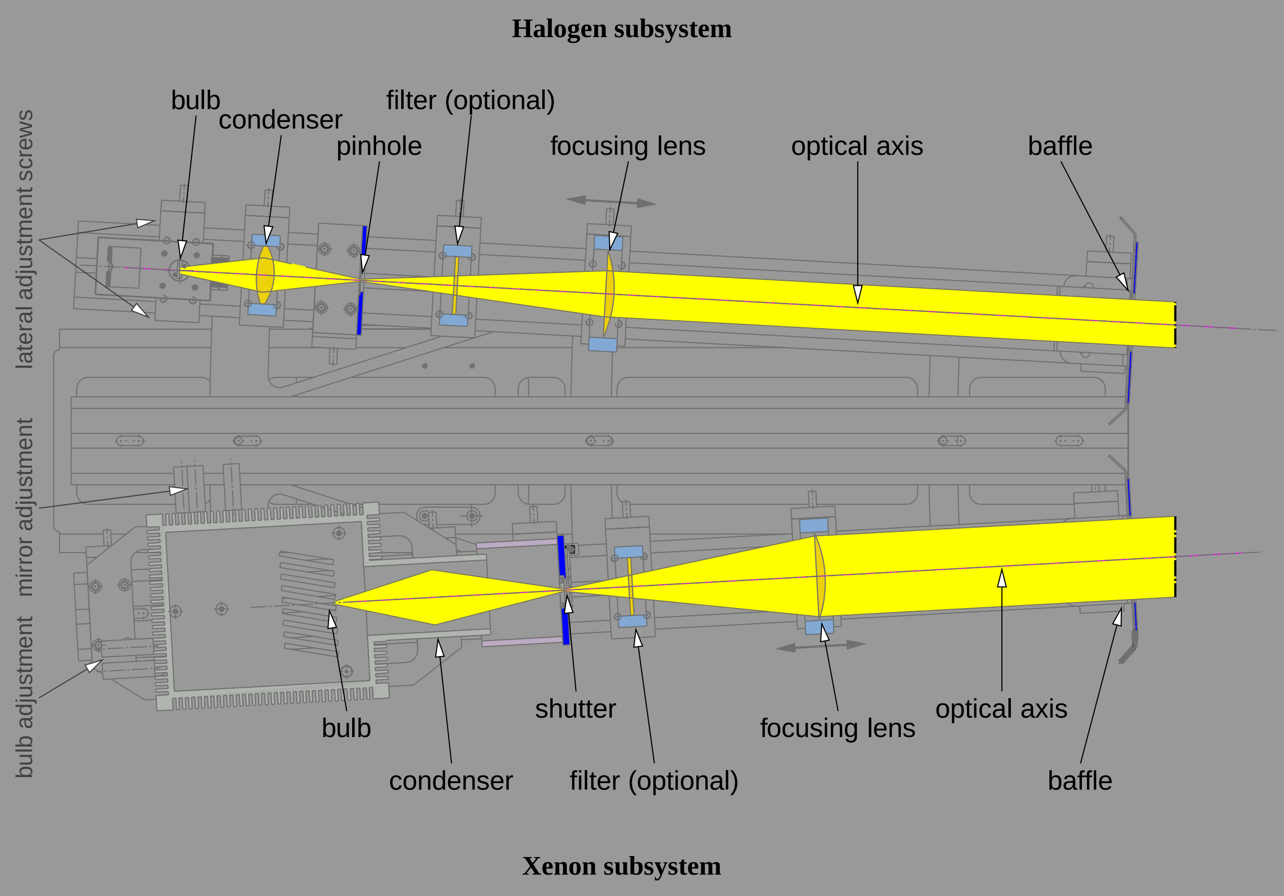
beam parameter	Halogen	Xenon	laser diode	gas laser
power	+	++	-	-
radiance	-	+	++	+++
noise	++	+	+	+
polychromatic	+	+	-	-
incoherent	+	+	-	-

choice depends on:

- sample type
- wavelength range
- detector type

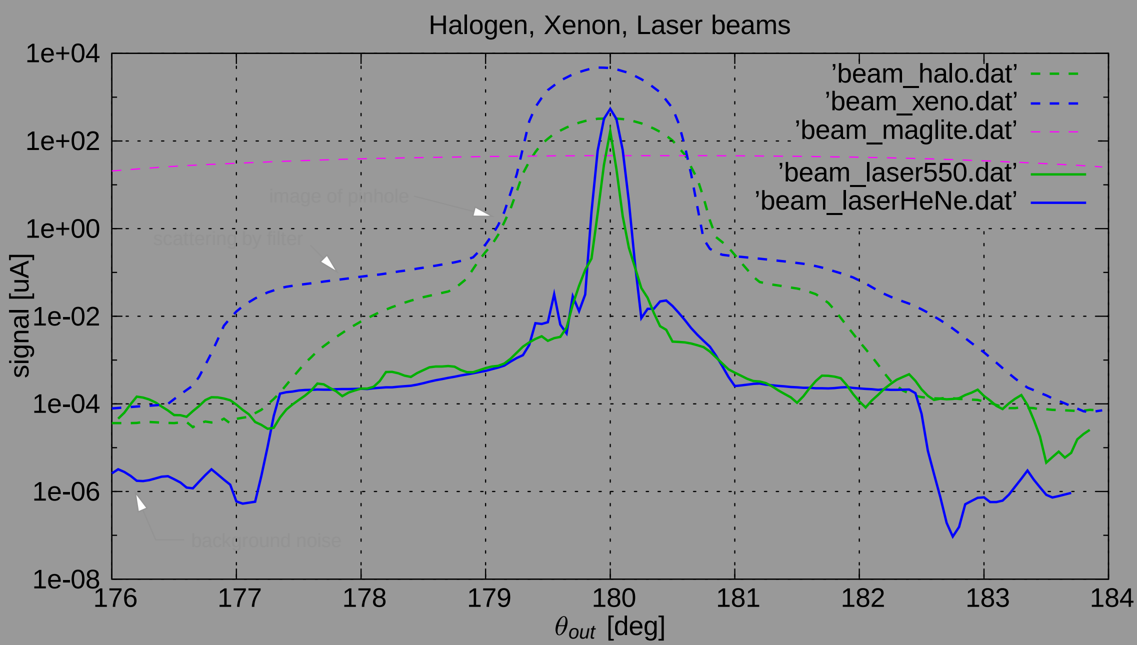
in the following: lamps kept at fixed positions
alternative concepts: moving lamp, fixed sample

example: pgII lamp subsystem



example: pgII lamp subsystem

example: beam profiles

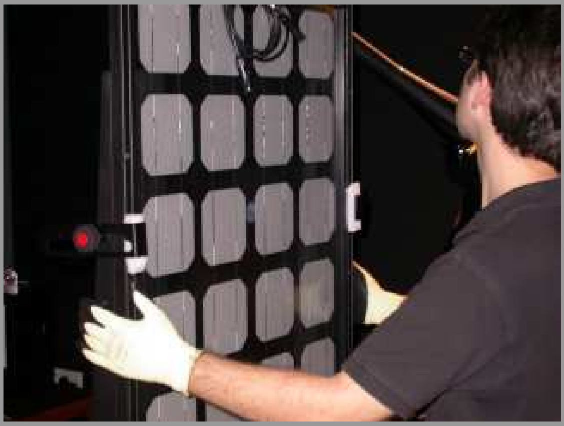
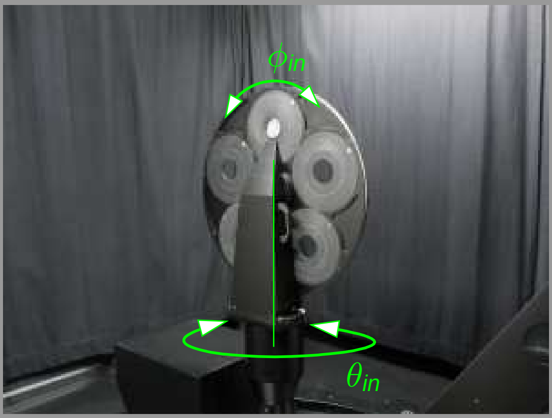


sample mount

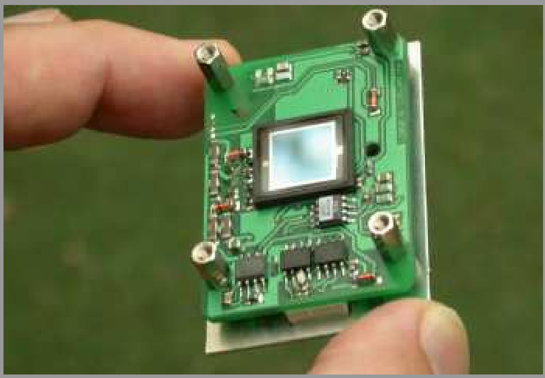
- fixes sample (securely)
- adjusts for θ_{in}, ϕ_{in}
- $\rightsquigarrow$ two degrees of freedom
  manual adjustment or automatic
- minimal self-shadowing
- shading of stray light

in the following: vertical sample mount assumed

example sample mounts

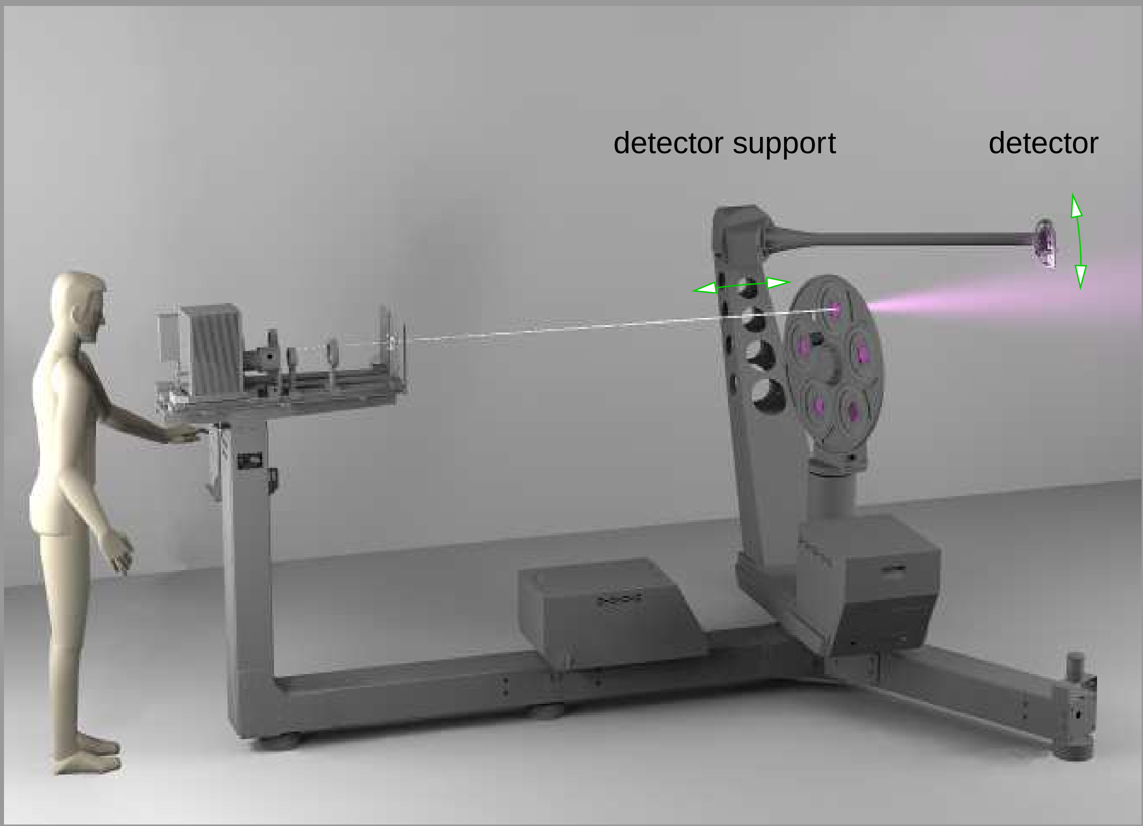




detector parameters

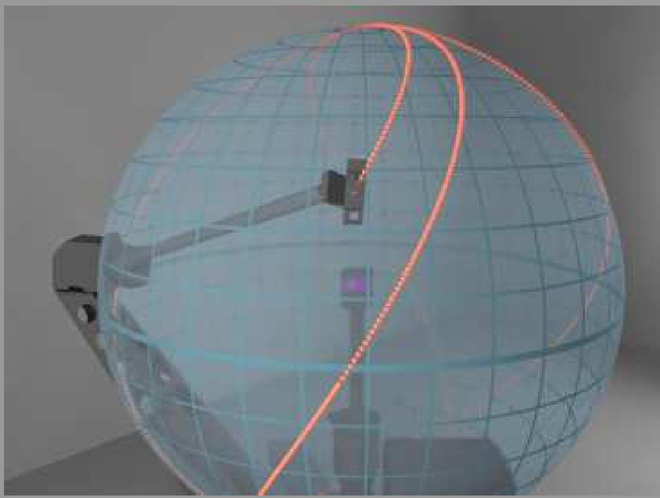


- material and wavelength: Si (VIS), InGaAs (IR), etc
- principle: photo-diode, etc
- sample rate: measurements / second: 1Hz to 1kHz
- noise: *noise equivalent BRTF*, lowest measurable BRTF
- dynamic range: 10^2 at least, 10^8 better

detector mechanics



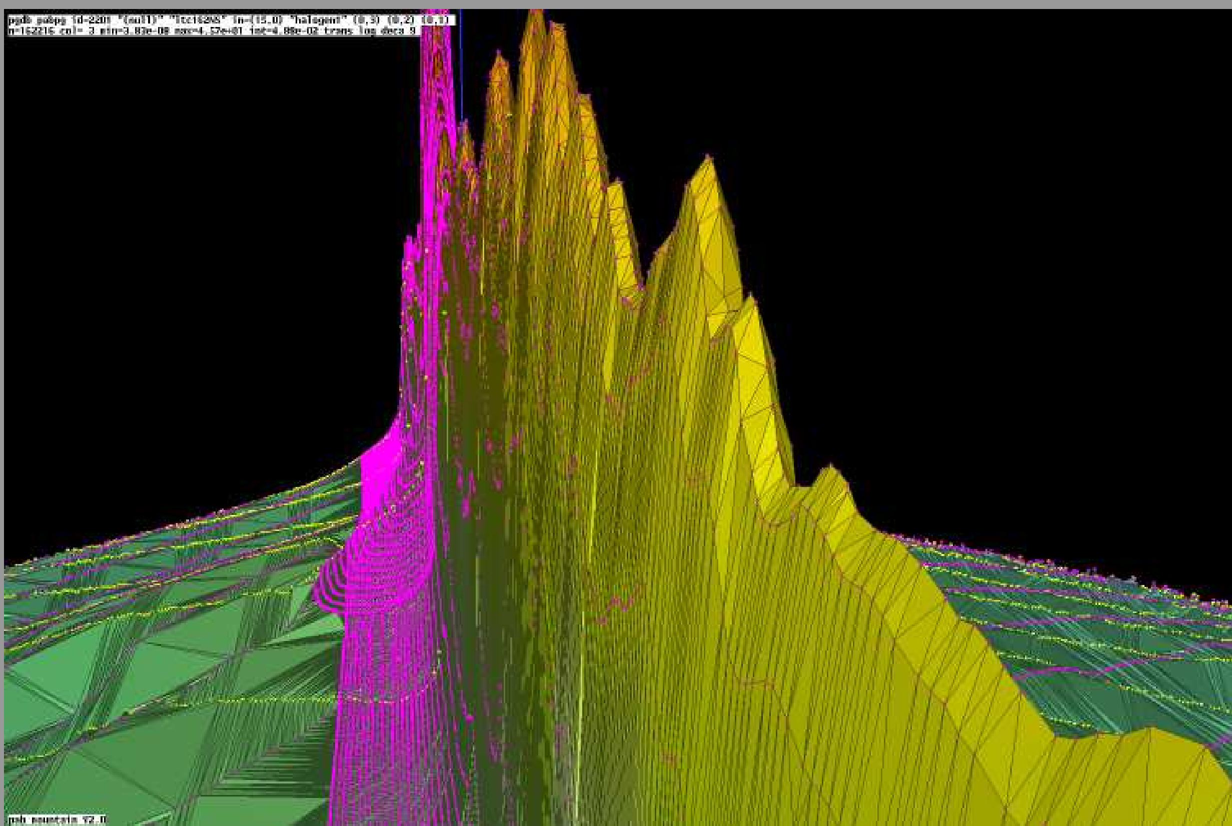
scanning gonio-photometer



measurements-on-the-fly:

- avoid start-stop-cycles
- need excellent sync between position and data-acquisition
- need fast detector

discrete BRTF values versus continuous function

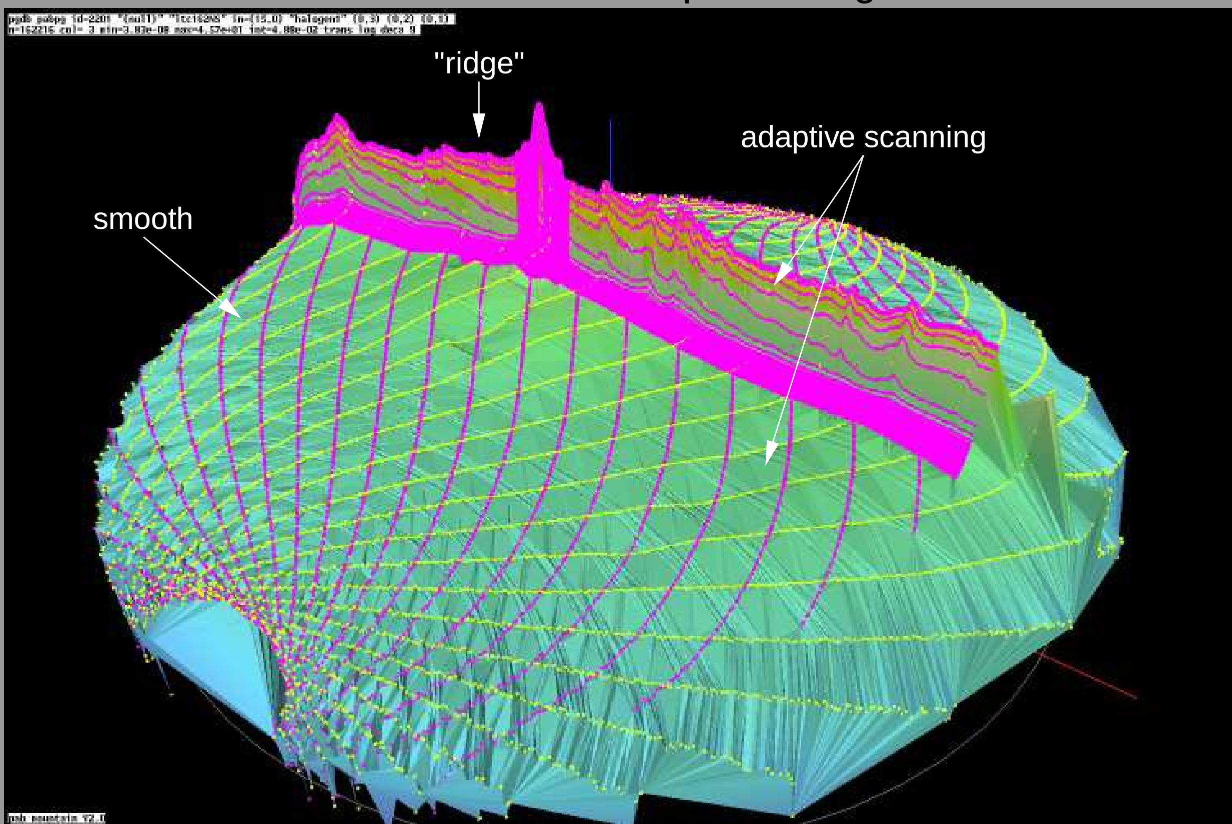


discrete BRTF values versus continuous function

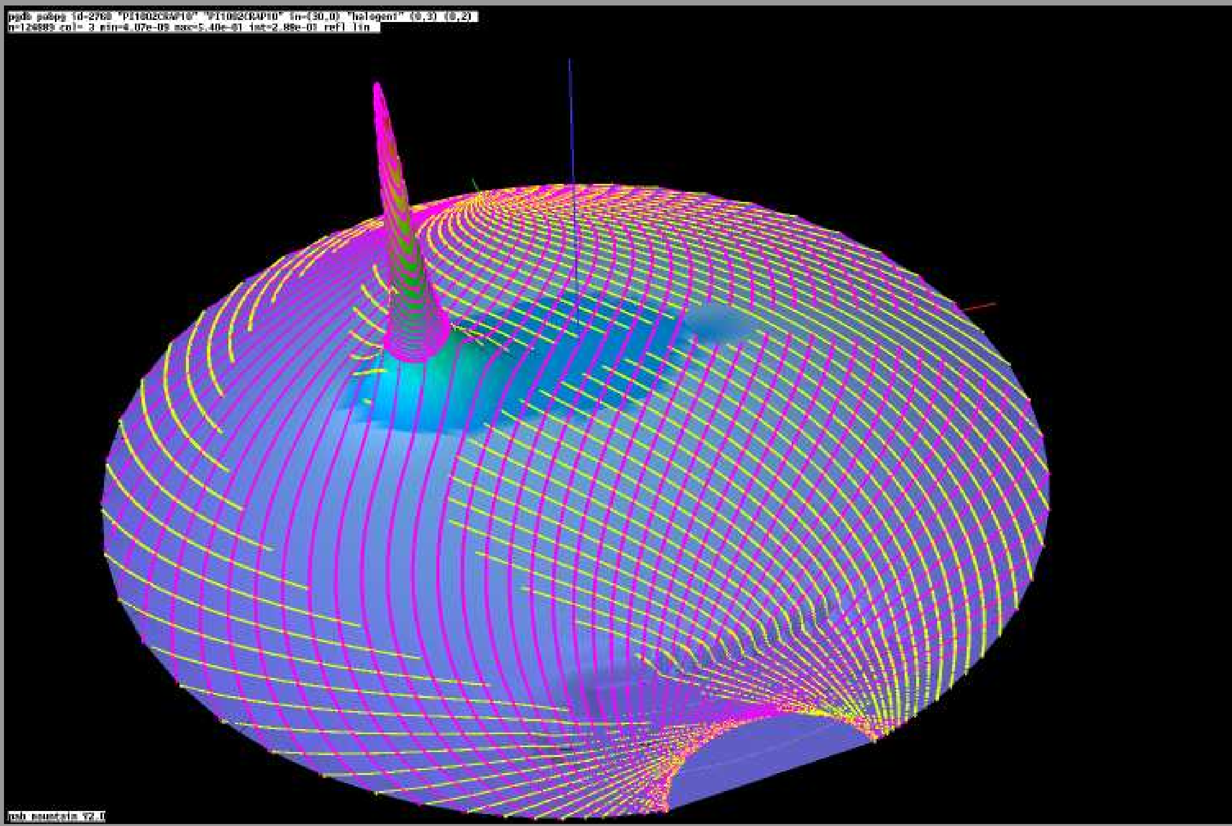
- in 3D, $f(x_i, y_i)$ data points
  do *not* define a unique surface
- Delaunay triangulation recommended
- triangulation used for interpolation and integration
- $\rightsquigarrow$ good triangulation vital for BRTF data processing

adaptive high angular resolution

BRTF consists of smooth areas and peaks/ridges:

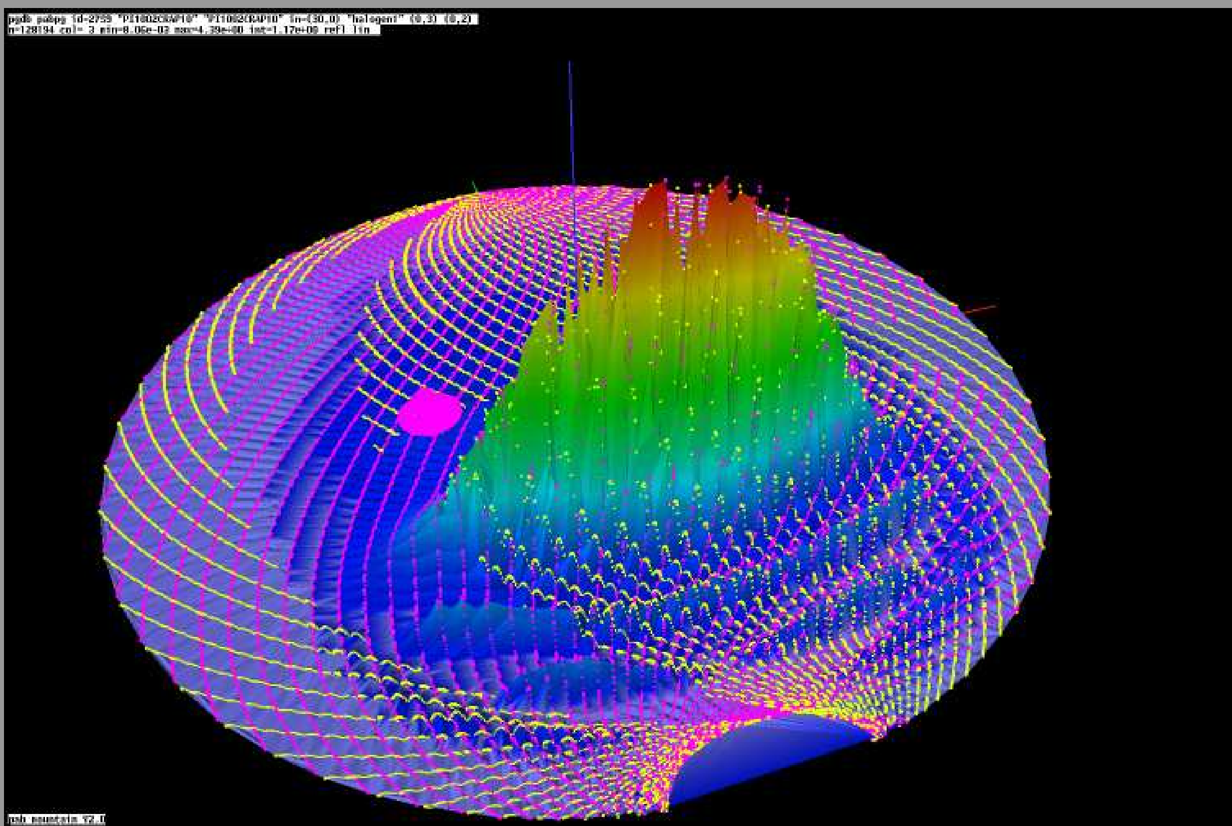


checking for measurement errors implicitly



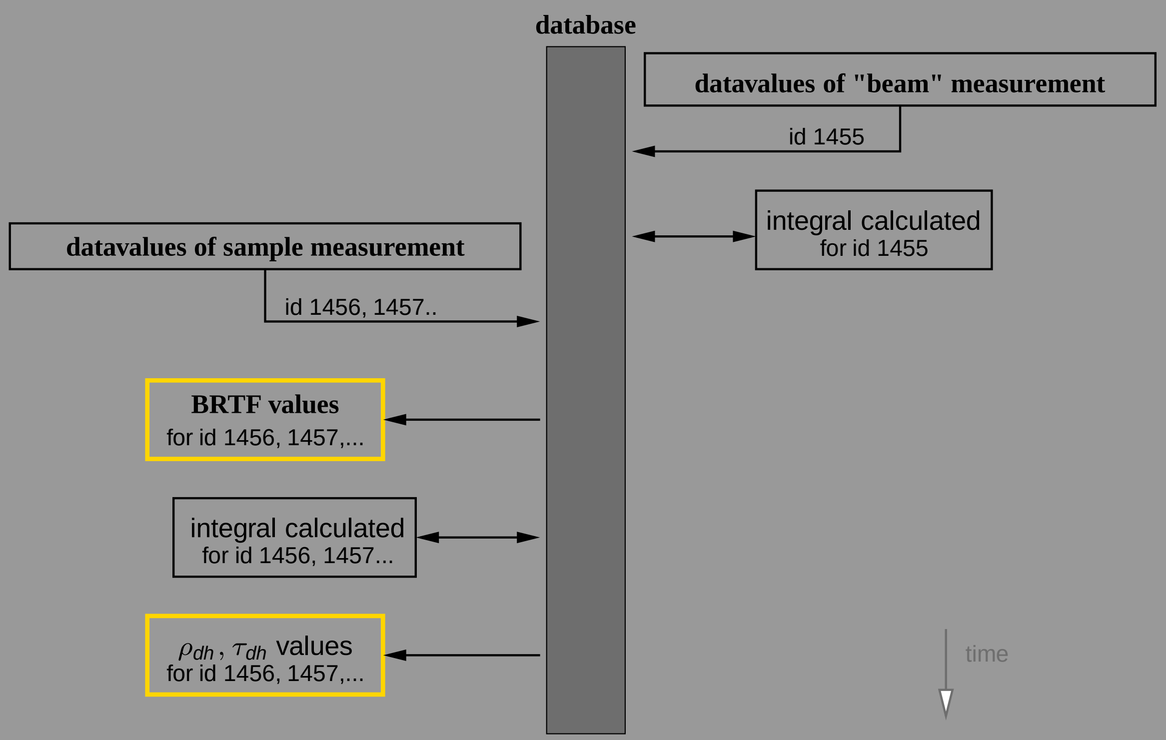
128109 data points all nicely smooth

checking for measurement errors implicitly



ceiling lights on, 100Hz noise, (see SPIE 2010 paper for more)

getting BRTF from raw data



getting BRTF from raw data

advantages of using unscattered beam as reference

- illuminated area and detector distance cancel out
- no reference samples needed
- sensor identical for reference measurement

imaging versus scanning gonio-photometers

alternative way of doing measurements:

imaging gonio-photometers

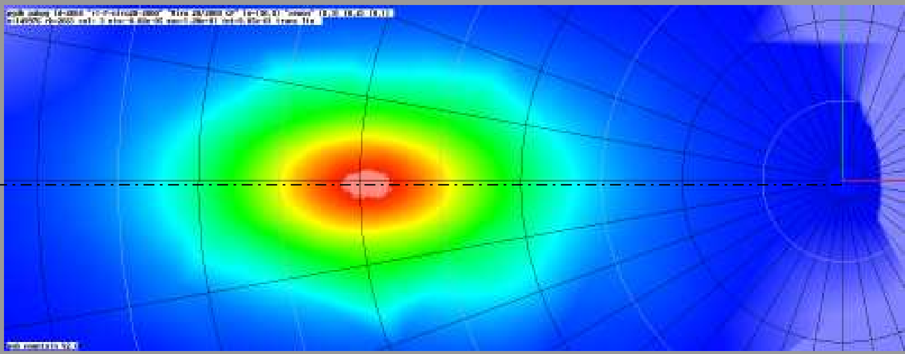
- + faster
- - more intermediate optics, not as general

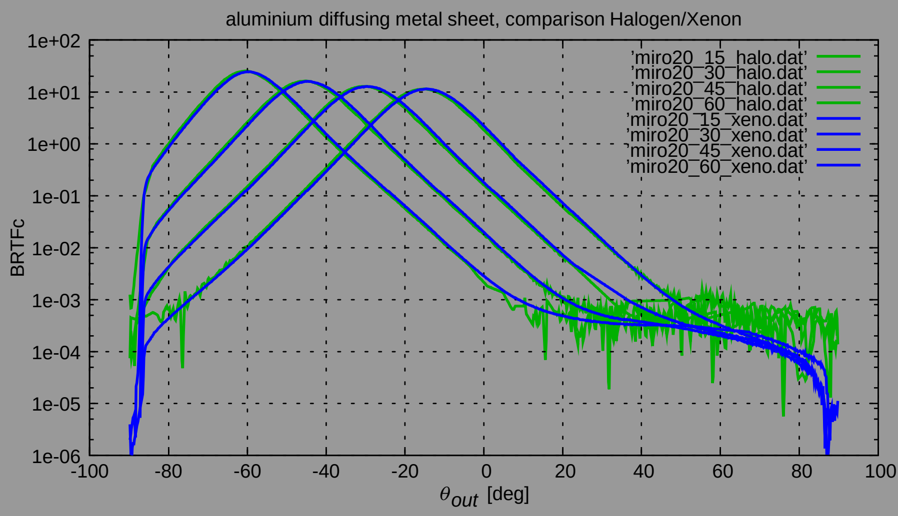
very short intermission

... questions to machine&measurement part ?

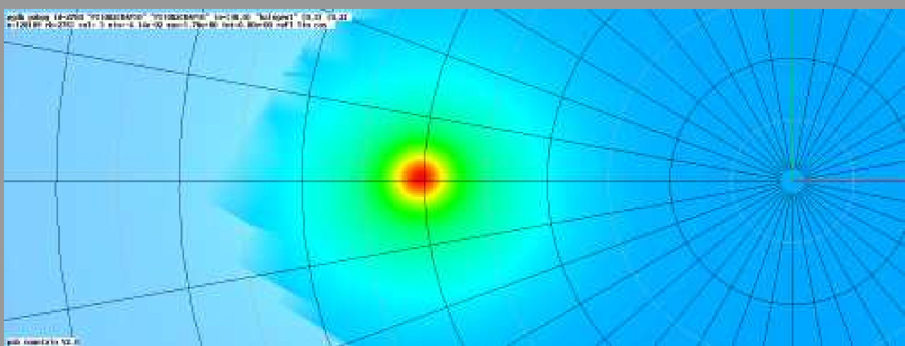
next to come: BRTF data &models

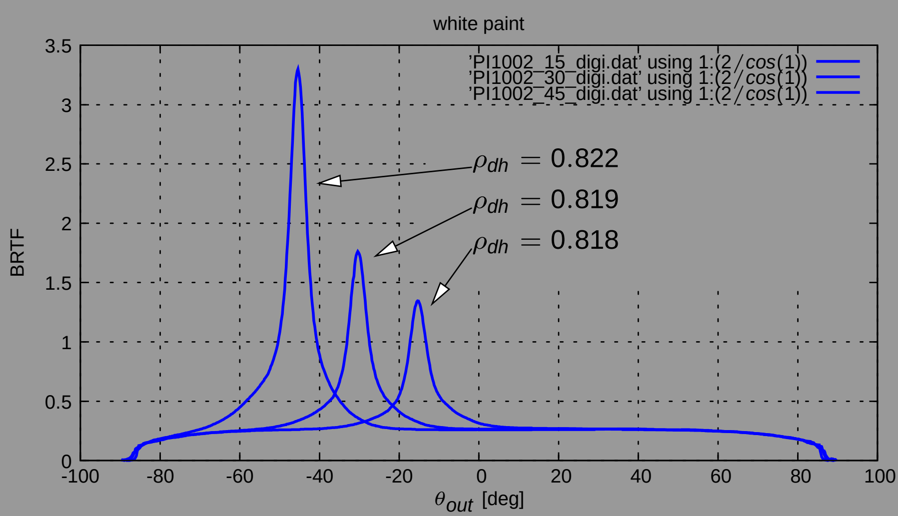
example: aluminium



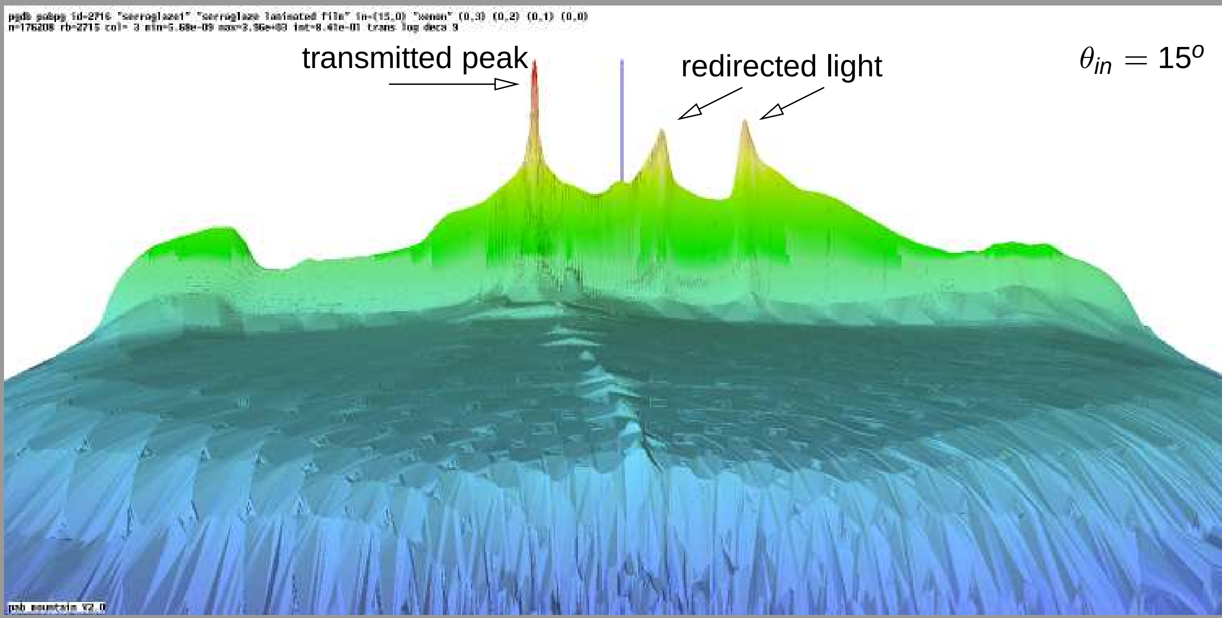


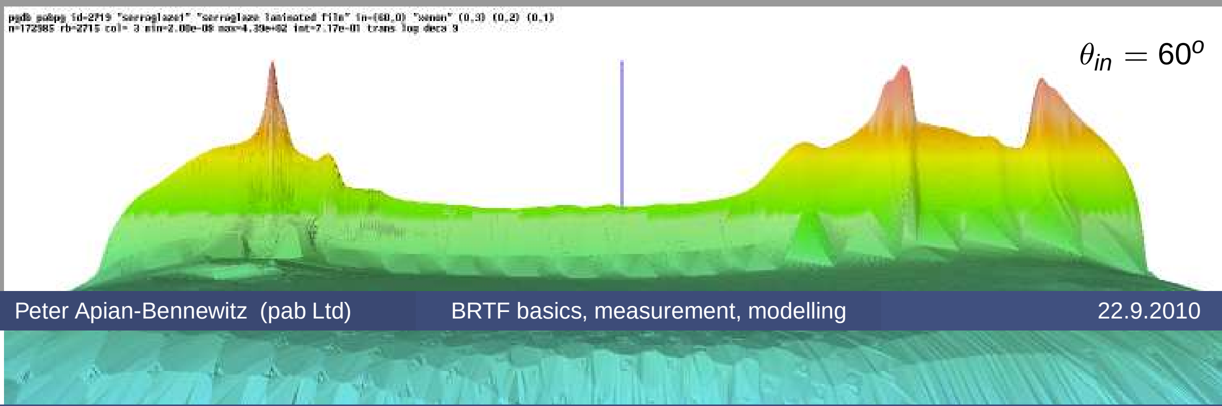
example: white paint





example: light redirecting, Serraglaze





angular resolution of incident and outgoing side

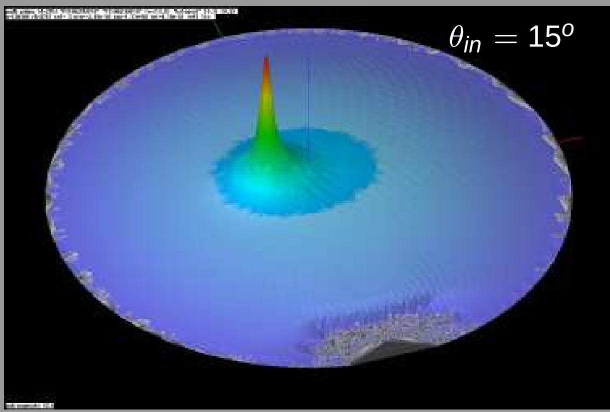
both sides are *not* symmetric:

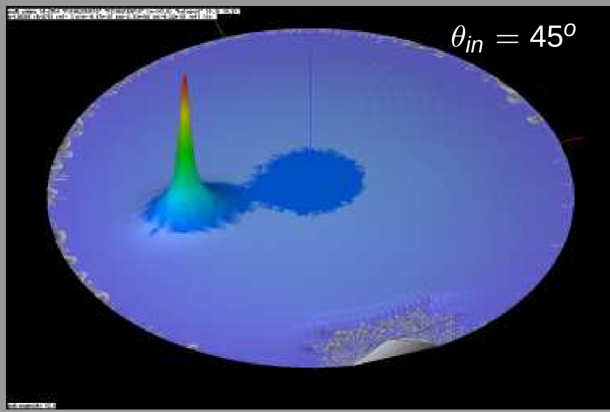
- outgoing side:
  adaptive, high resolution (0.1^o)
- incident side:
  low resolution (10^o)

since:

Theorem
in most cases the topology of a BRTF does not change between $\vec{x}_{in}$ and $\vec{x}_{in} + \Delta$, for small Δ (e.g. 20^o)

topology of a BRTF





- structure ("topology") of BRTF remains the same for Δ
- shape *parameters* change:
  peak position, peak height, peak width, background level
- $\rightsquigarrow$ intermediate θ_{in} are predictable.
- $\rightsquigarrow$ measurements of finely resolved θ_{in} are redundant
- $\rightsquigarrow$ don't waste time and data with these
  think of a good interpolation method

getting BRTF into *Radiance*

problems to solve while importing data:

- interpolation between outgoing directions $\vec{x}_{out}$:
  triangulation, etc
- interpolation between incident directions $\vec{x}_{in}$:
  not a trivial problem
- optional data compression

ways into simulation program

- loading BRTF data-files directly
- fitting of parameters of internal model (`trans, plastic`)
- fitting of parameters of external model (`cal` files)
- loading of compressed/processed data

loading BRTF data-files directly

problems:

- adaptive scans produce non-grid data
- `brightdata, brtfdata` expect data on regular grids (depends on index function, but index into 100k points is cumbersome)
- no interpolation between incoming directions
- $\rightsquigarrow$ direct import is de-facto not supported

alternative way: interpolate data to regular grid

- coarse grid misses peaks
- fine grid increases memory requirements
- $\rightsquigarrow$ not a solution

fitting parameter of function to BRTF data

process:

- fit $f_{a_1...a_N}(\theta_{out}, \phi_{out})$ to one dataset of incident direction $\vec{x}_{in}$
- $\rightsquigarrow$ set of parameters $a_1...a_N$ or each (θ_{in}, ϕ_{in})
- use functions g_i to fit a_i to (θ_{in}, ϕ_{in})
- $\rightsquigarrow$ model complete for outgoing and incident directions
- best situation: a_i simple function of (θ_{in}, ϕ_{in})

drawbacks:

- requires that f and choice of $a_1...a_N$ describe scattering well
- requires thinking for each material. not automatic.
- standard Levenberg-Marquardt method not 100% robust

note: see chapter 5 in author's 1995 dissertation (in German)

choice of model function

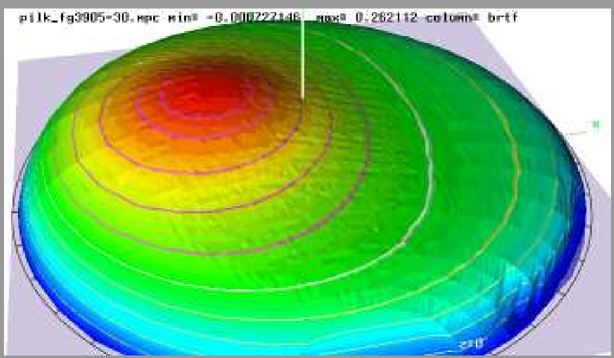
- internal to *Radiance* (e.g. `trans`)

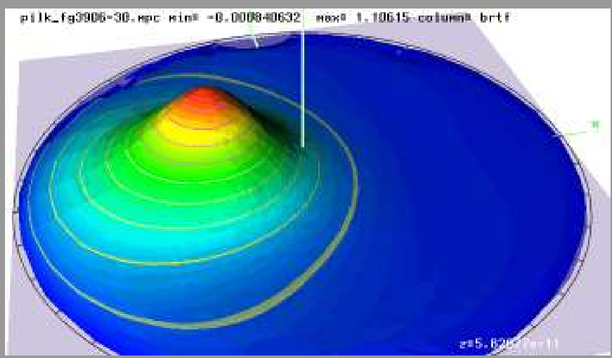
$$BRTF_{trans} = \frac{a_6\,(1-a_7)}{\pi} + \frac{a_6\,a_7}{\pi a_5^2\,\sqrt{\cos(\theta_{in})\cos(\theta_{out})}}\exp[(2\,\cos(\theta_{half})-2)/a_5^2] \quad (6)$$

- external (example)

$$\begin{aligned} BRTF_{cosgauss} &:= a_1 + a_2(\cos\theta)^{a_3} + a_4\exp(-\beta^2\,a_5) \quad (7)\\ \beta &:= \arccos[\cos(\theta)\cos(\alpha_{in}+a_6) - \sin(\theta)\cos(\phi_{out})\sin(\alpha_{in}+10a_6)]\\ \theta &:= \pi - \theta_{out} \end{aligned}$$

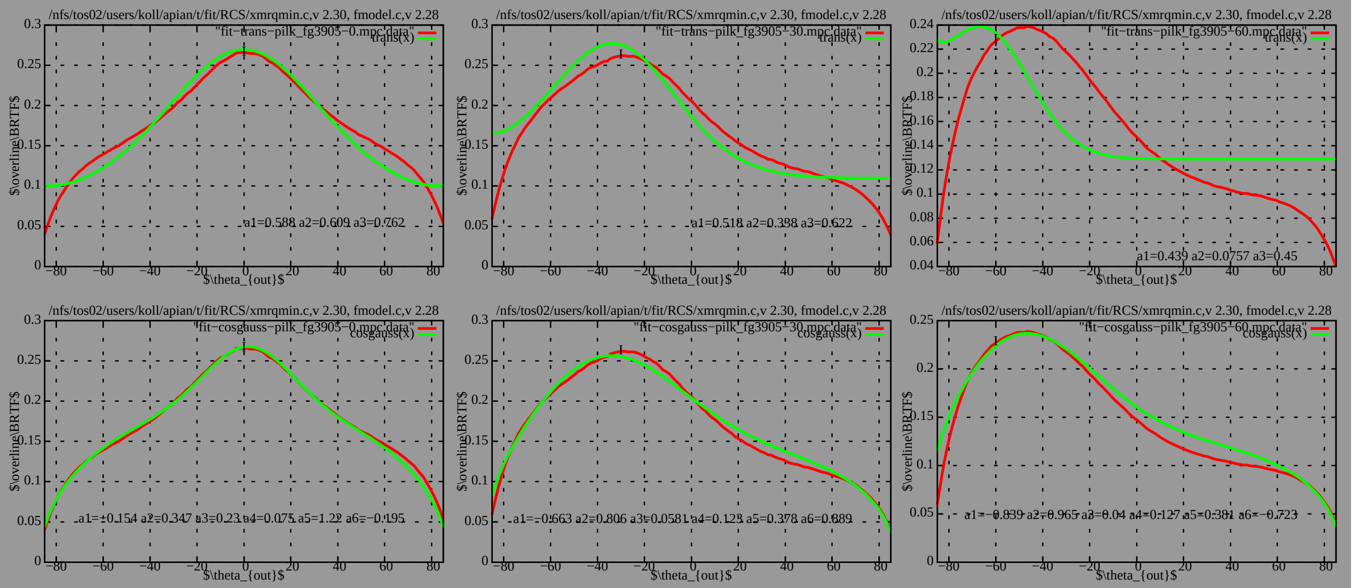
example: fits to Pilkington fg3905, fg3906 in 1994





polymer/glass sandwich glazing,
forward scattering, ”milky” glazing

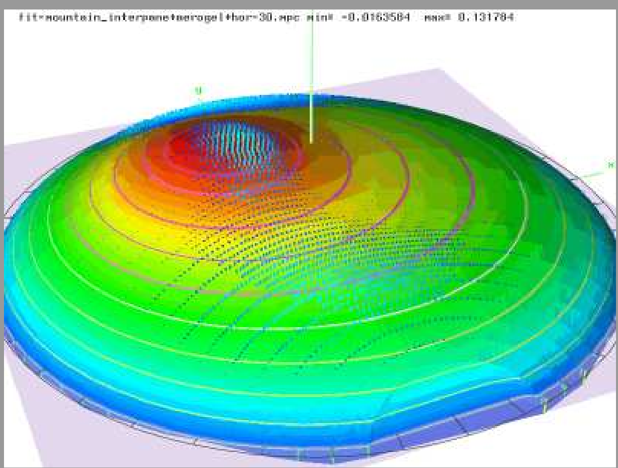
fg3905 model comparison, in scattering-plane

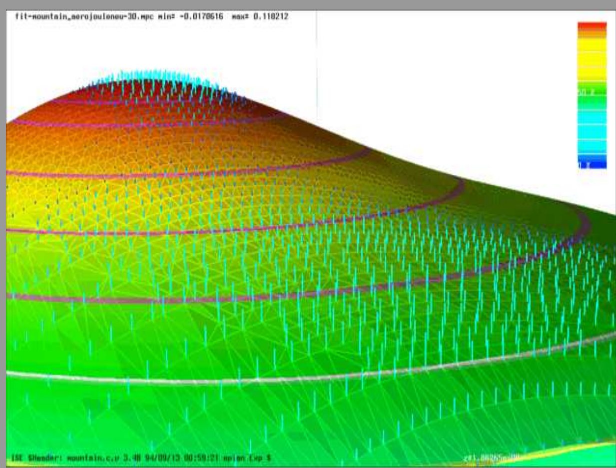


red curves: measured data , green curves: BRTF model
top row: *trans* material, $\theta_{in} = 0, 30, 60^o$
bottom row: suggested *cosgauss* model (cal file), $\theta_{in} = 0, 30, 60^o$

note: see chapter 6 in author's 1995 dissertation for details

fg3905 model comparison, off scattering-plane

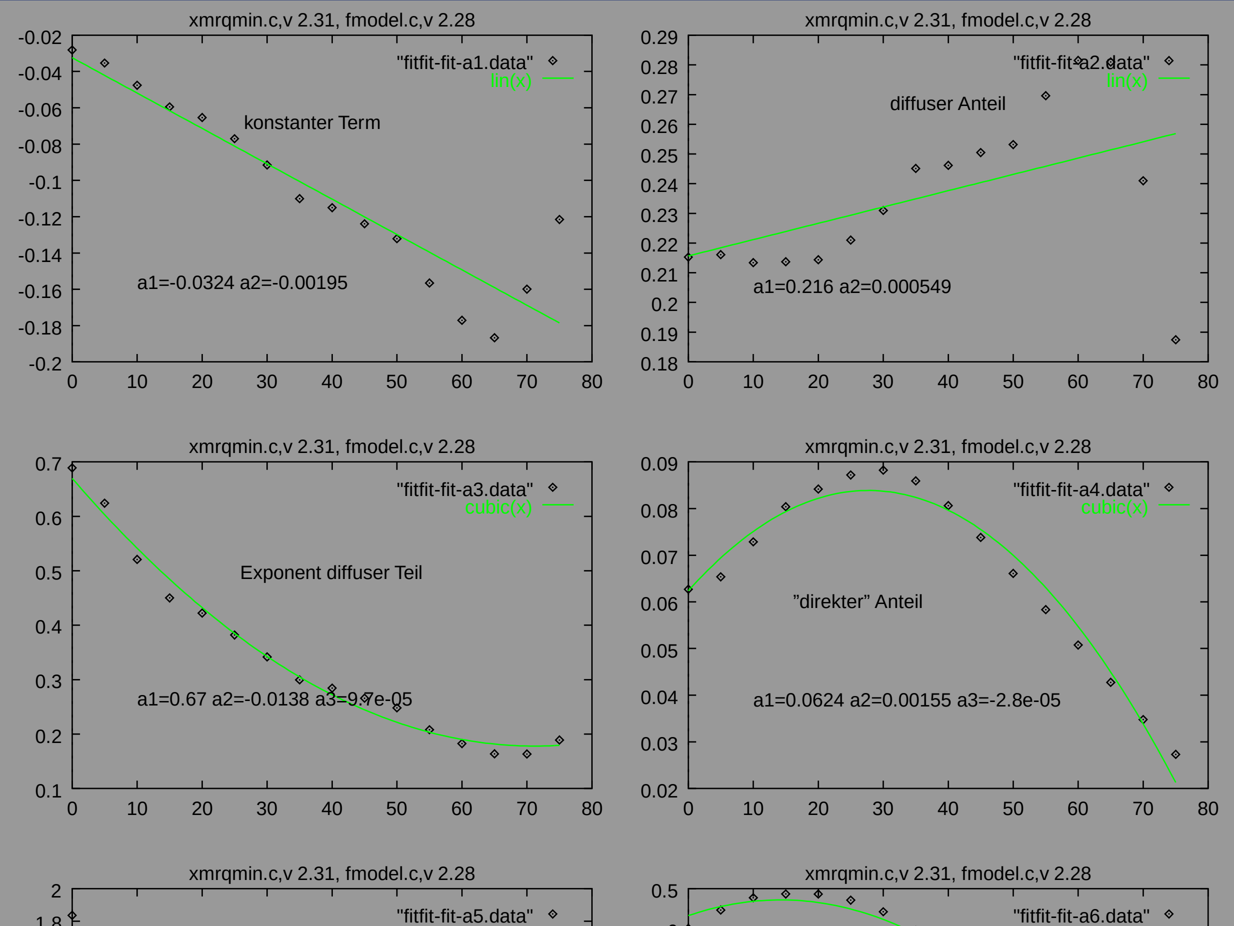


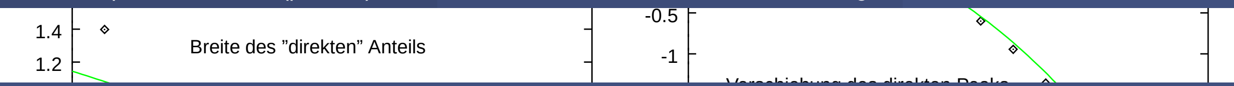


deviation between model and data shown as spikes

fitting is done for *all* outgoing directions (not just in-plane)
model may deviate more outside the scattering plane

example: Aerogel model, parameter variation





conclusions for *Radiance* models

- current models don't match measured data well
- better built-in models or cal-files seem worth considering

what *Radiance* is missing

- *cal* file support for photon-map (and ambient calcs)
  $\rightsquigarrow$ support for general BRTF models
- BRTF import using non-fixed-grid data
- way to add internal models in a modular way
  (equivalent to a complete rewrite)

all these features require changes to the rendering core

$\rightsquigarrow$ non trivial work. But would be *very* useful in practice.

...thanks

last slide.

- physics is fun
- happy rendering
- thank you for joining workshop and thanks for your attention

links

latest papers on pgII gonio-photometer & links:

- ”Experimental validation of bidirectional reflection and transmission distribution measurements of specular and scattering materials,”
  SPIE 2010, Brüssel, http://dx.doi.org/10.1117/12.854011
- ”New scanning gonio-photometer for extended BRTF measurements”
  SPIE 2010, San Diego, http://dx.doi.org/10.1117/12.860889
- currently installed pgII gonio-photometers:
  SERIS Singapore, LBNL Berkeley, pab Freiburg, industrial client Europe
- pgII gonio-photometer webpage:
  http://www.pab.eu
- author’s 1995 Phd: http://www.pab-opto.de/pers/phd/

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